

Mitigating Top-Down Cracking in Asphalt Pavements

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Outline

- Introduction
- Scope of Study
- Volumetric Properties
- Material Properties
- Energy Ratio
- Summary & Conclusions



Focus on the Energy Ratio Concept, Development & Results



Introduction

- Top-down cracking is recognized as a major form of distress in HMA.
- 90% of pavements scheduled for rehab:
 - Deficient crack rating
 - Top-down cracking
- FDOT - UF embarked on a multi-year study to identify causes and solutions.



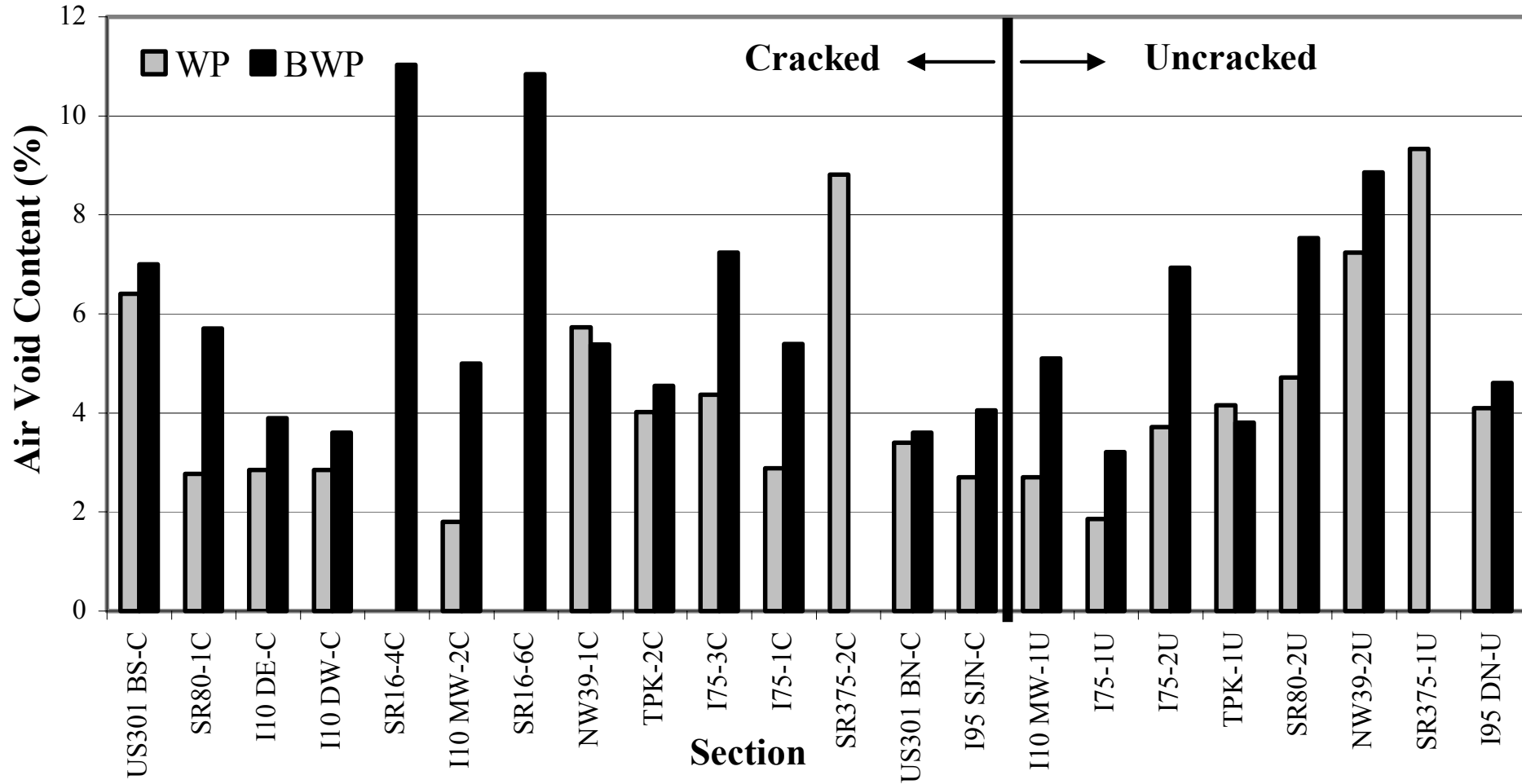
Scope of Study

- 25 field test sections to-date
 - Continuing study w/ 12 additional planned
- Comprehensive evaluation:
 - Volumetric properties
 - Material properties
 - Effect of traffic loads and tires
 - Pavement structure (pavement design)



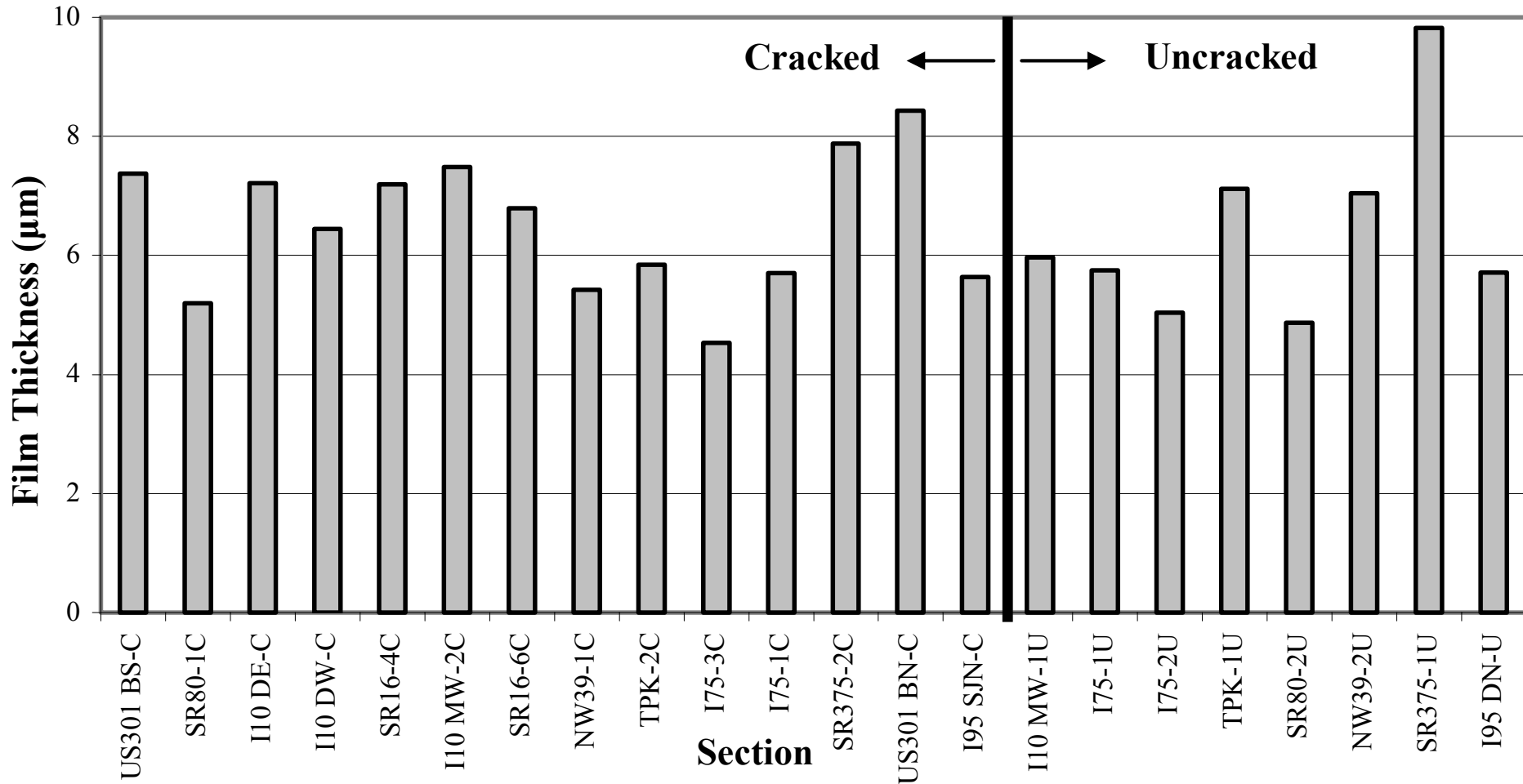
Air Voids

- WP cores showed lower AV% than BWP



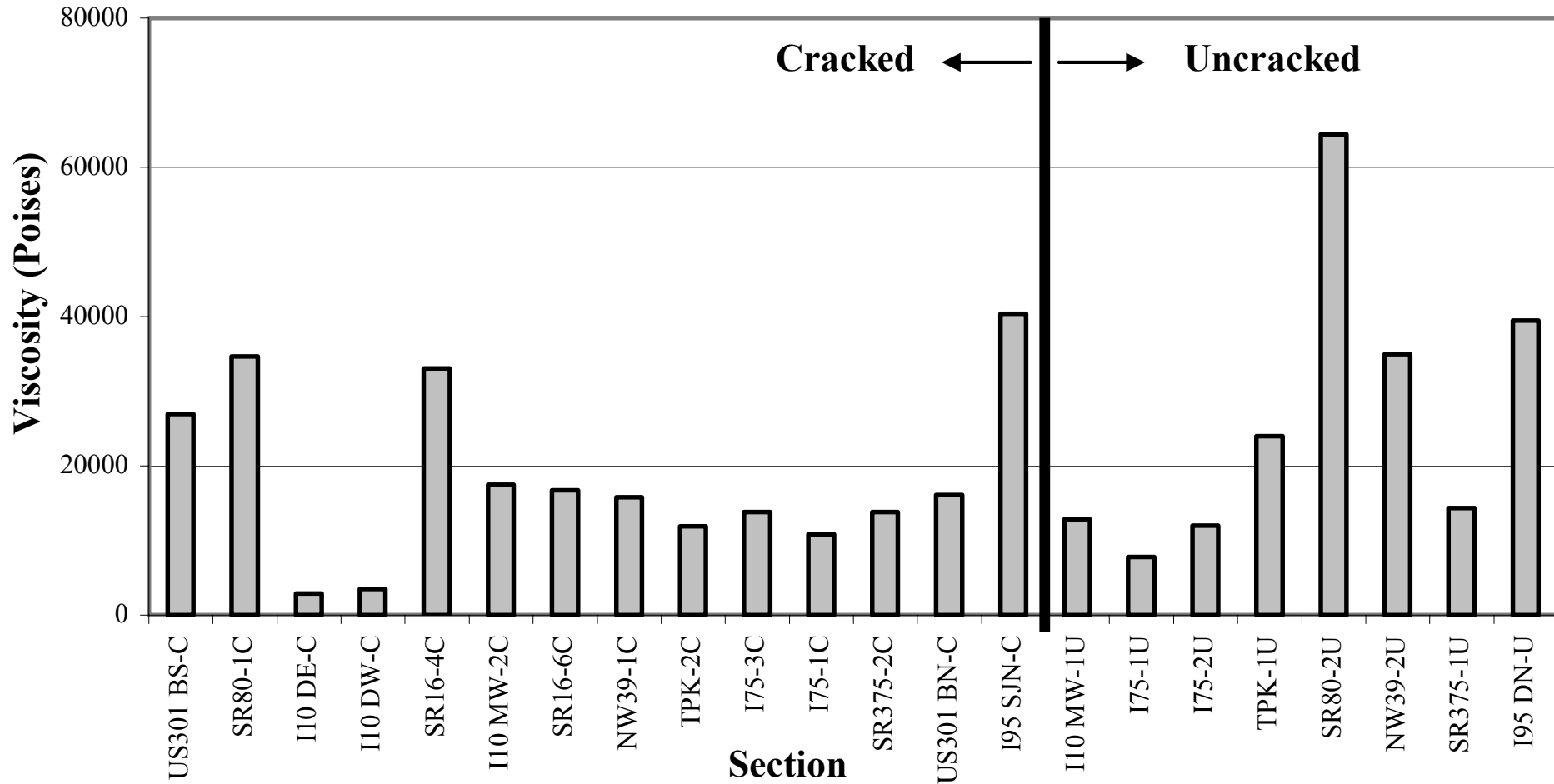
Theoretical Film Thickness

- Proposed minimum 9-10 μm [Kandhal]



Binder Viscosity

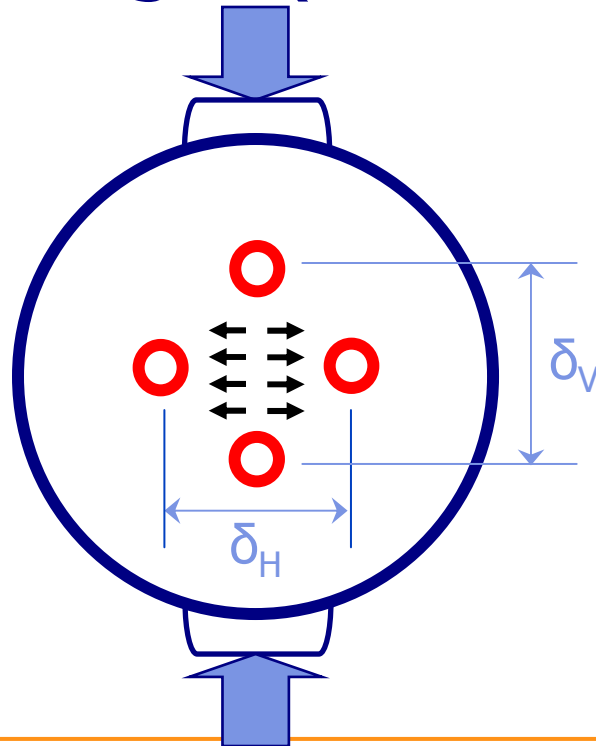
- Age hardening



Mixture Properties

Superpave indirect tensile test:

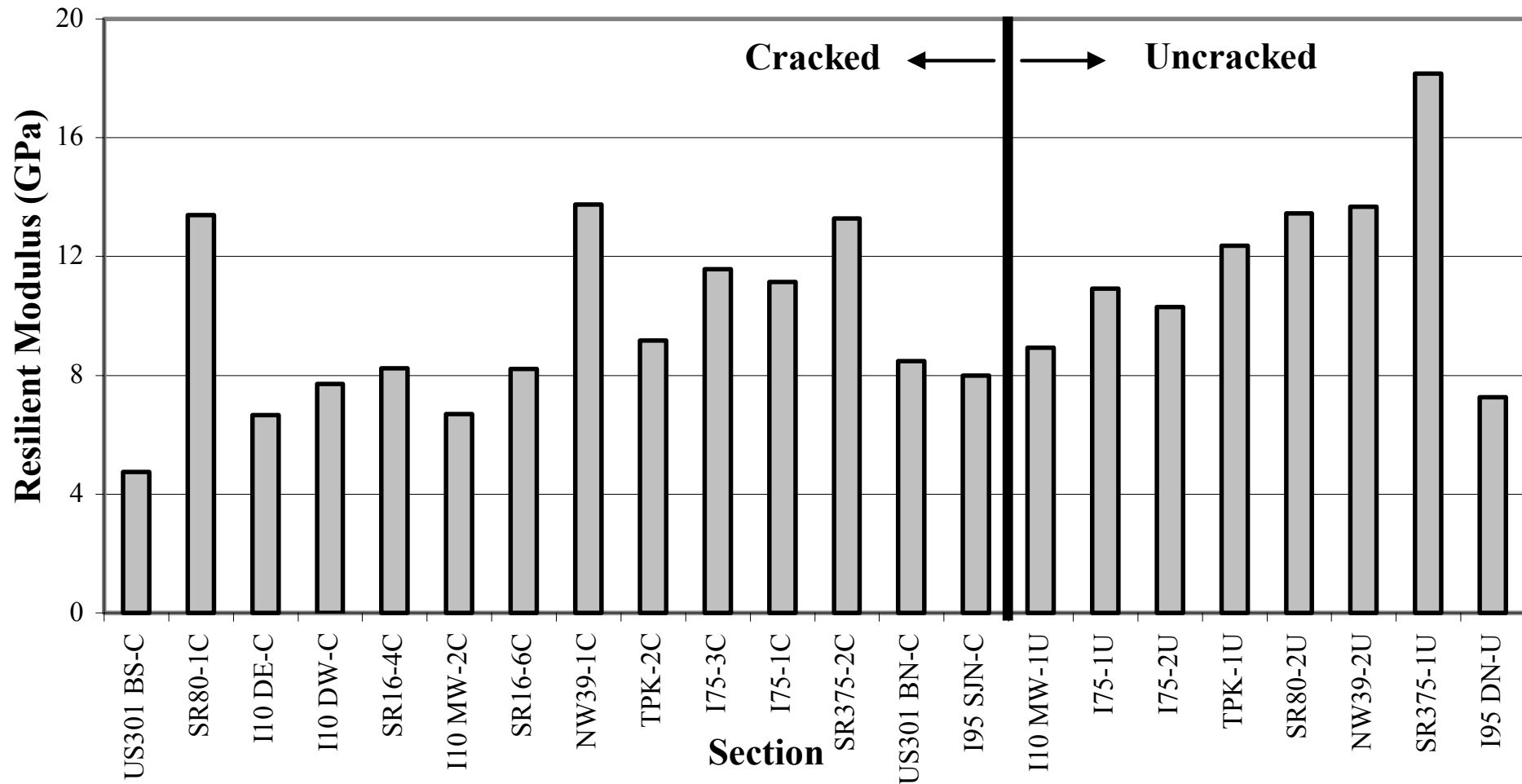
1. Resilient modulus (Cyclic loading)
2. Creep (Constant load with time)
3. Strength (Increase load until fracture)



- Apply vertical load
- Measure vertical & horizontal deformations

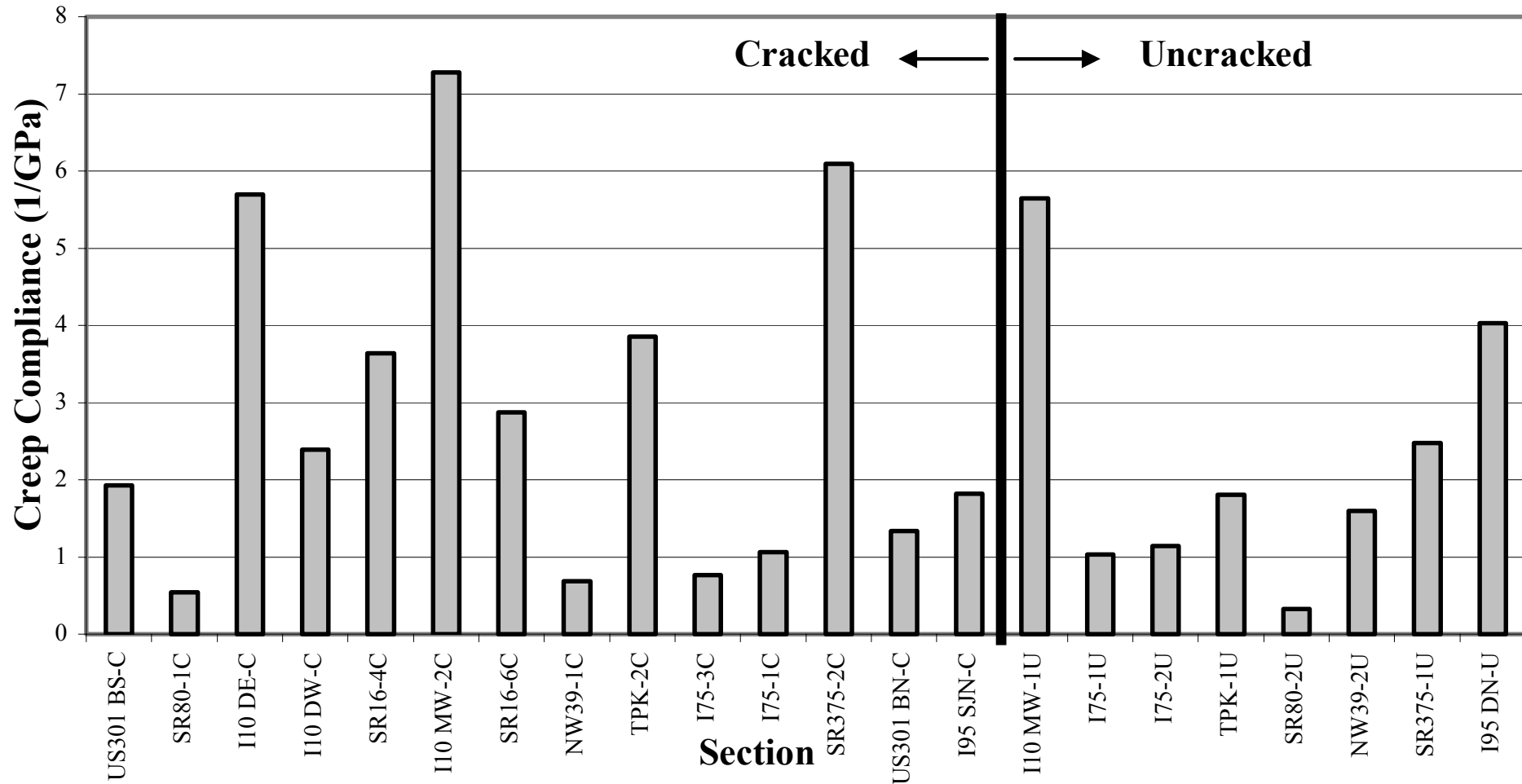
Resilient Modulus

- Measure of elastic stiffness



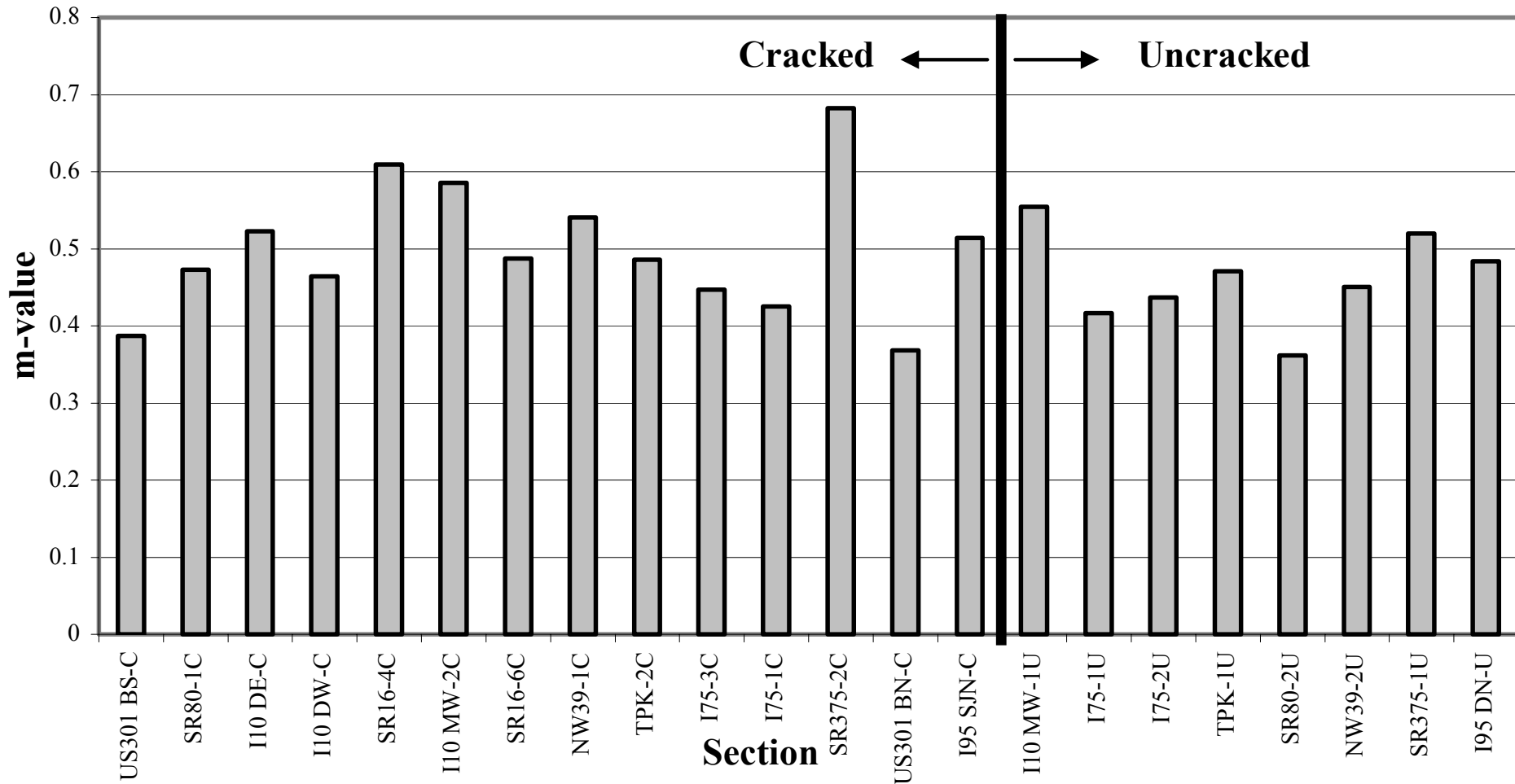
Creep Compliance

- Ability of the mixture to relax stresses



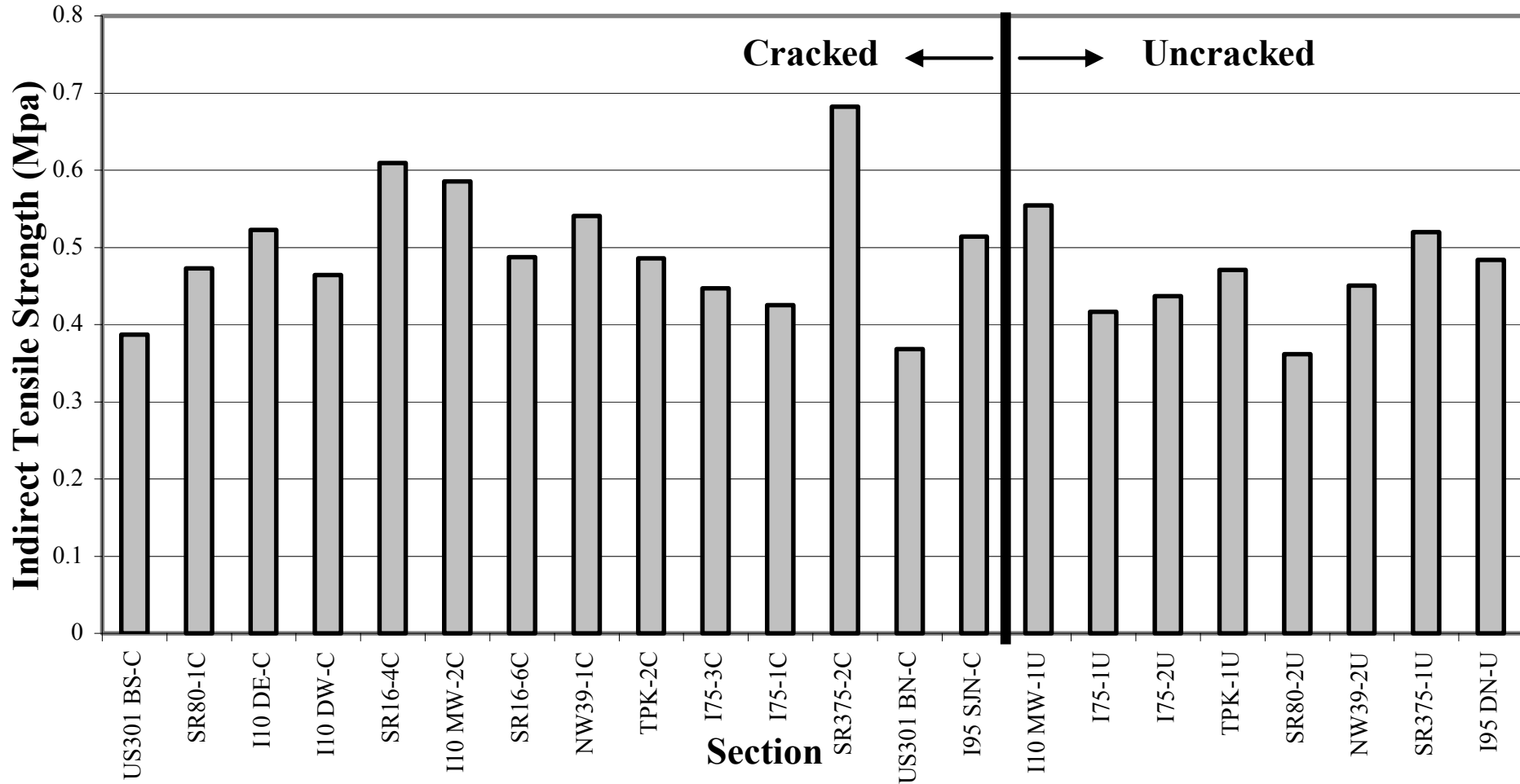
m-Value

- Measurement of creep rate (rate of damage)



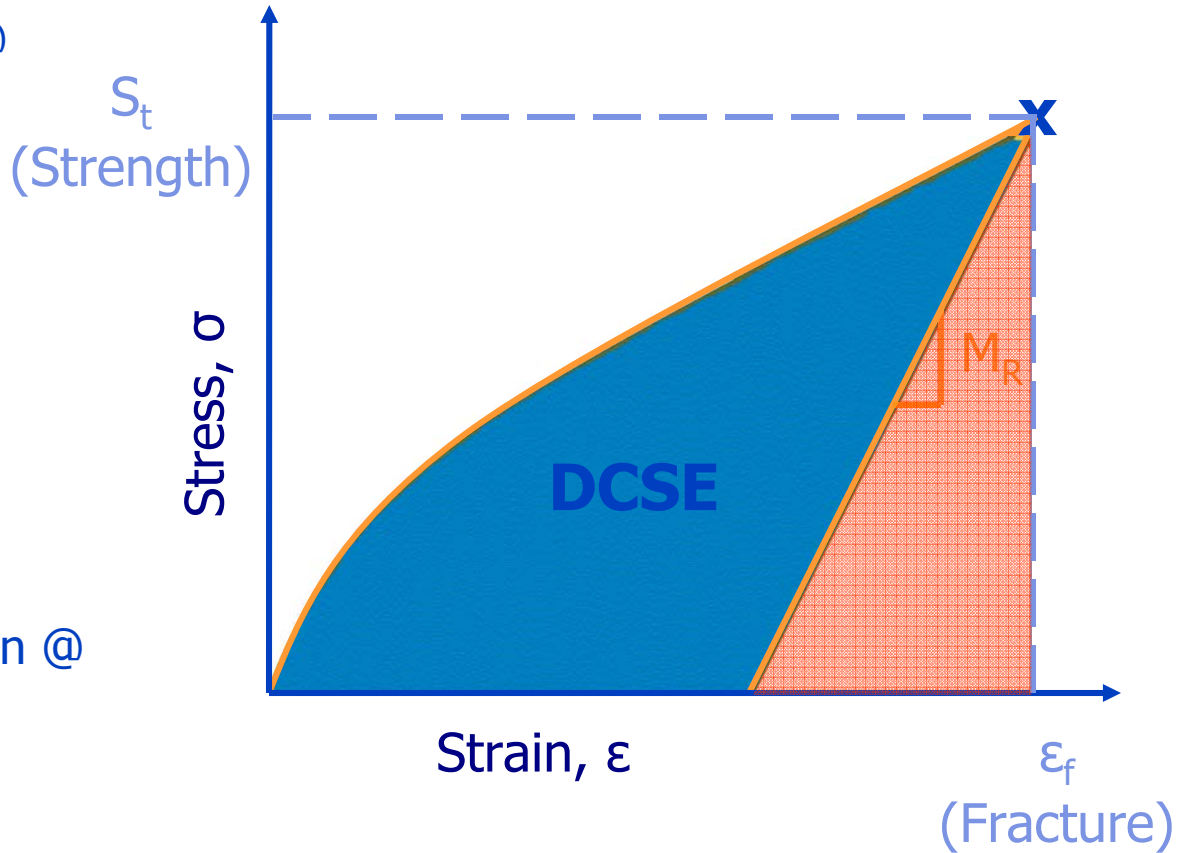
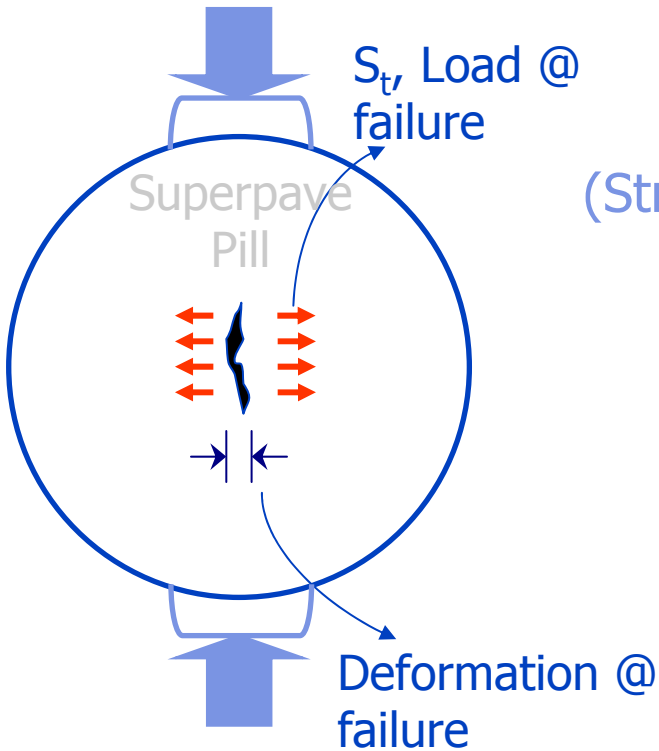
Tensile Strength

- Maximum tensile stress before failure

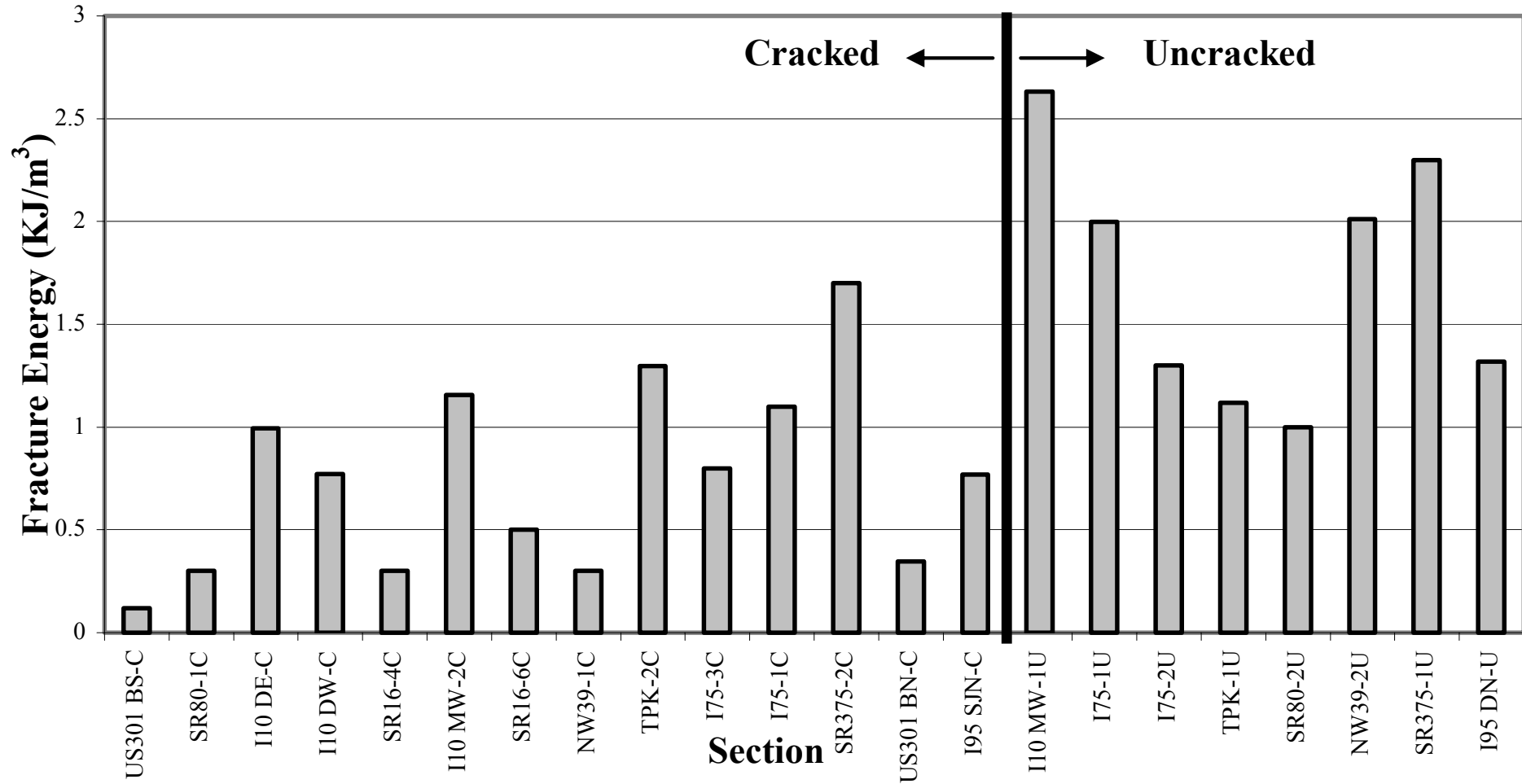


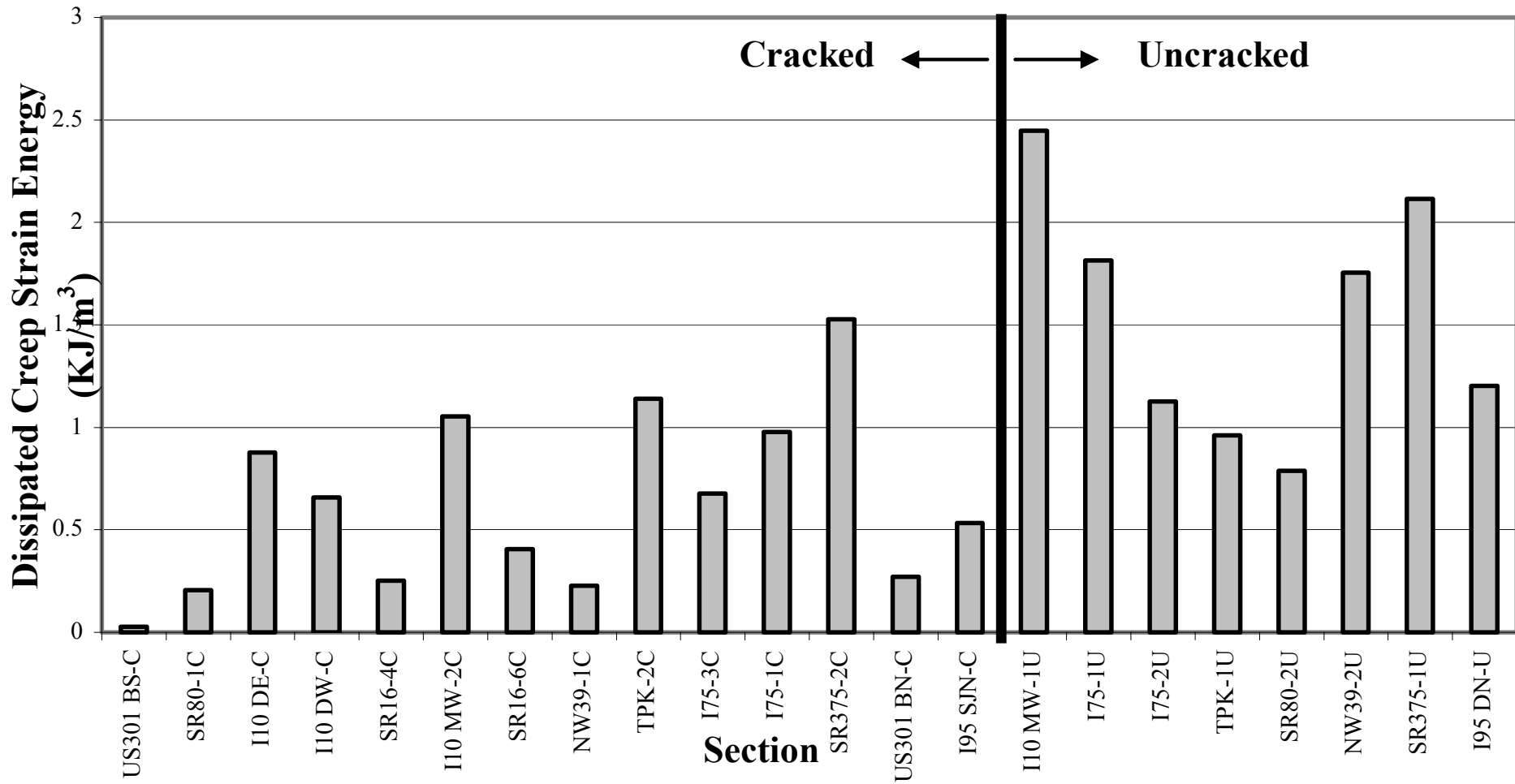
Dissipated Creep Strain Energy

Based on the M_R and Strength tests



Fracture Energy (FE)





What is missing?

- Energy by itself did not accurately predict the performance of all sections
- Need to introduce a model that predicts cracking performance based on material properties (from IDT creep test) and pavement structure characteristics (predicted tensile stress)



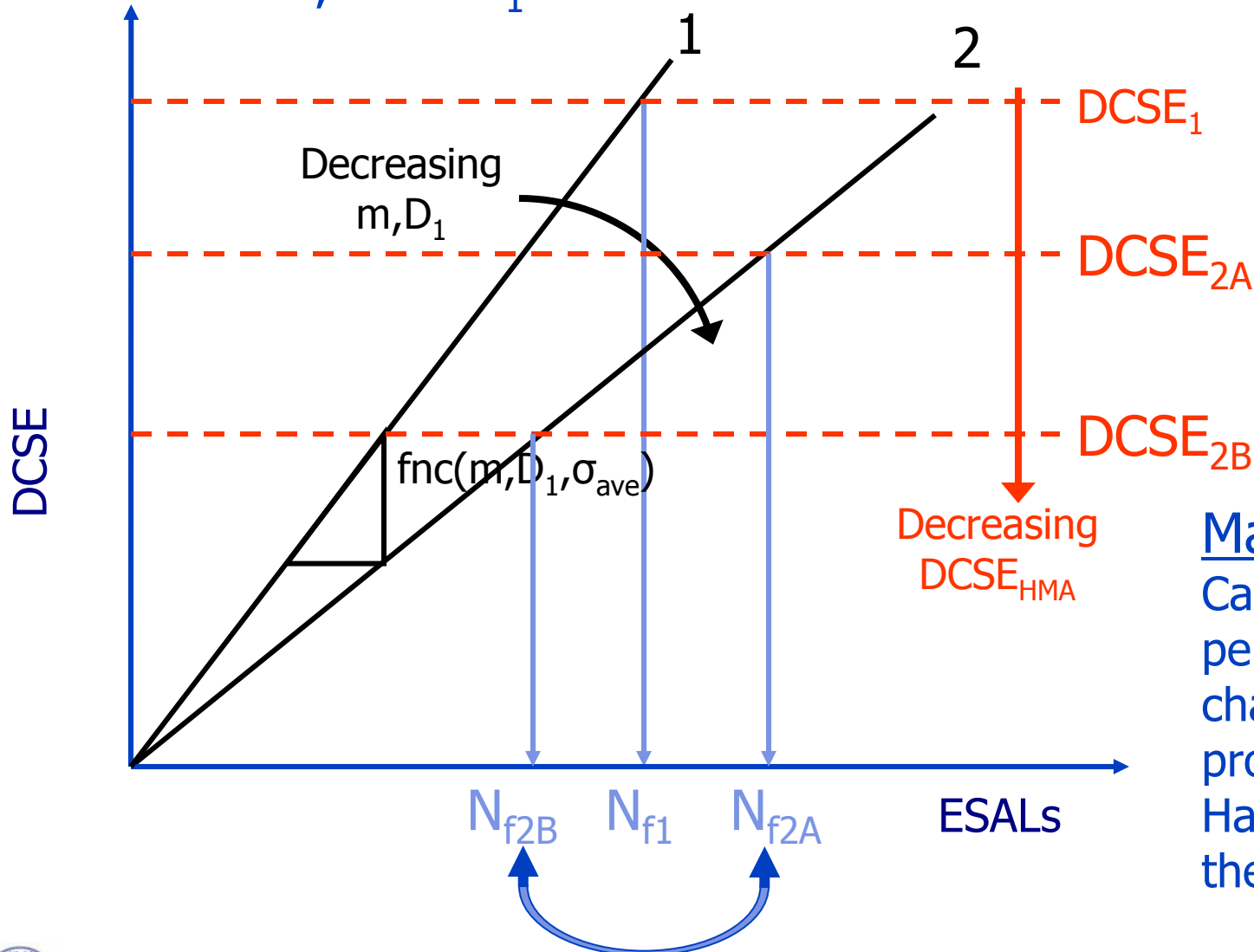
HMA Fracture Model

- Calculates the crack growth for a given level of applied stress
- Using:
 - Material properties – m , D_1 & $DCSE_f$
 - Structural properties – σ_{AVE}



HMA Fracture Model

DCSE, m & D_1 are interrelated

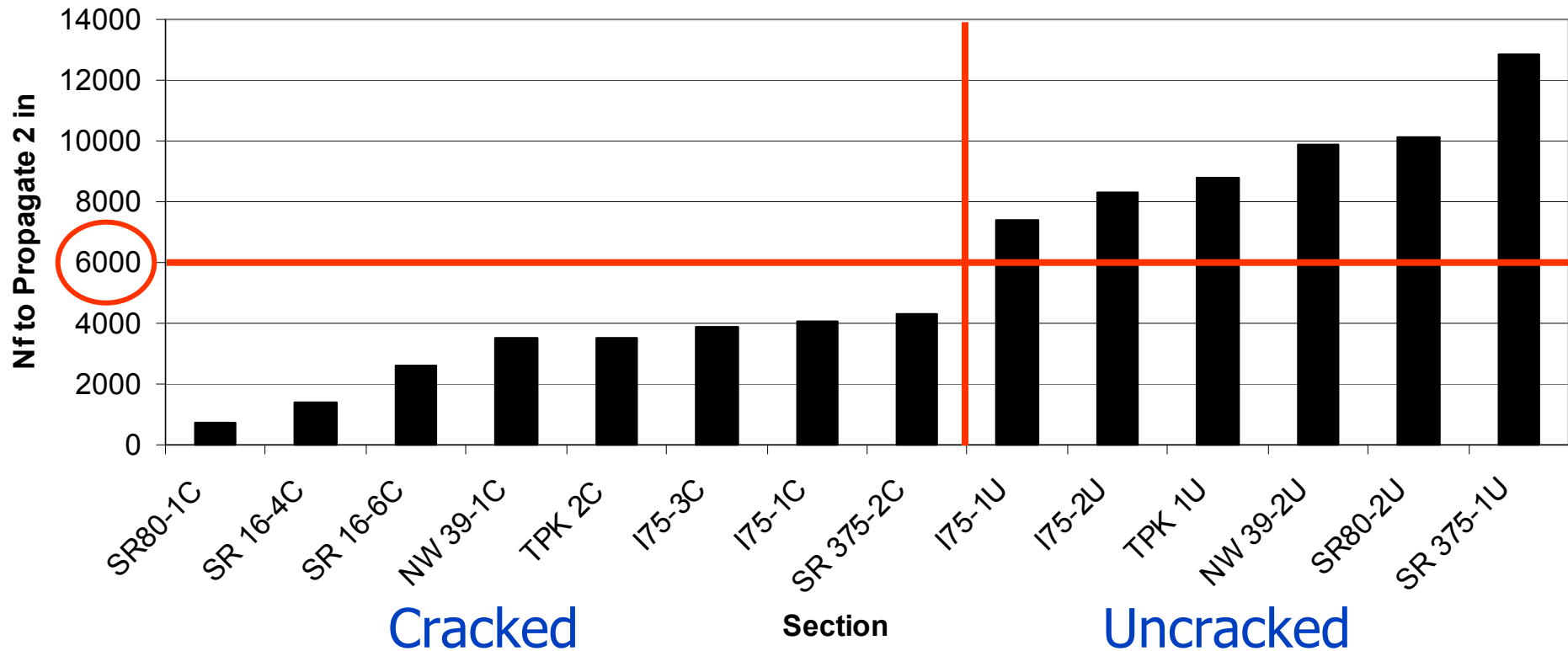


Main Idea:
 Can not improve performance by changing a single property.
 Have to consider the entire system.



Cycles to Failure

- Used the HMA Fracture Model to calculate N_f for crack to propagate 2 in



- Mixtures with $N_f < 6000$ performed poorly



Minimum Energy

- $DCSE_{min}$ is the minimum energy required to produce $N_f=6000$
- Express the $DCSE_{min}$, D_1 & m-value relation in a single function:

$$- DCSE_{min} = \frac{m^{2.98} D_1}{A}$$

$$- A = \frac{(6.36 - S_t)}{33.44 \times \sigma_t^{3.1}} + 2.46 \times 10^{-8}$$

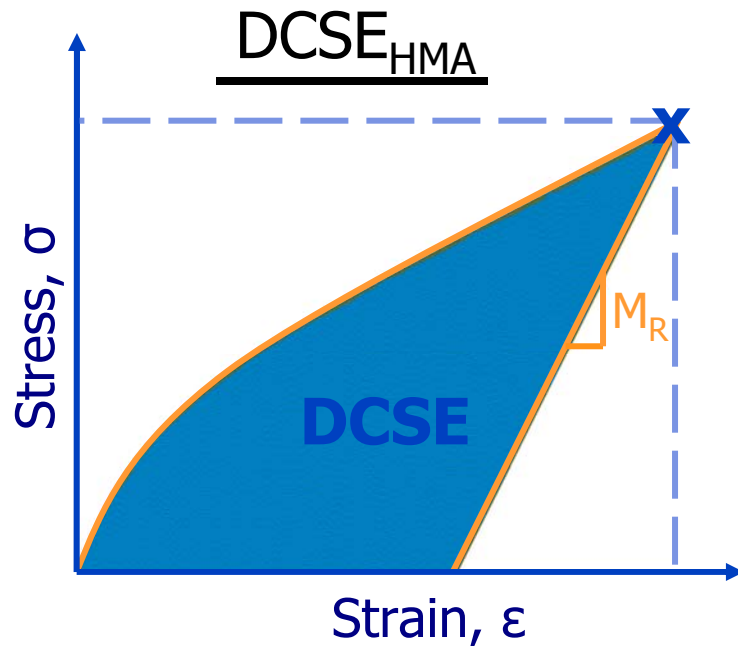
S_t = Tensile Strength

σ_t = Tensile Stress

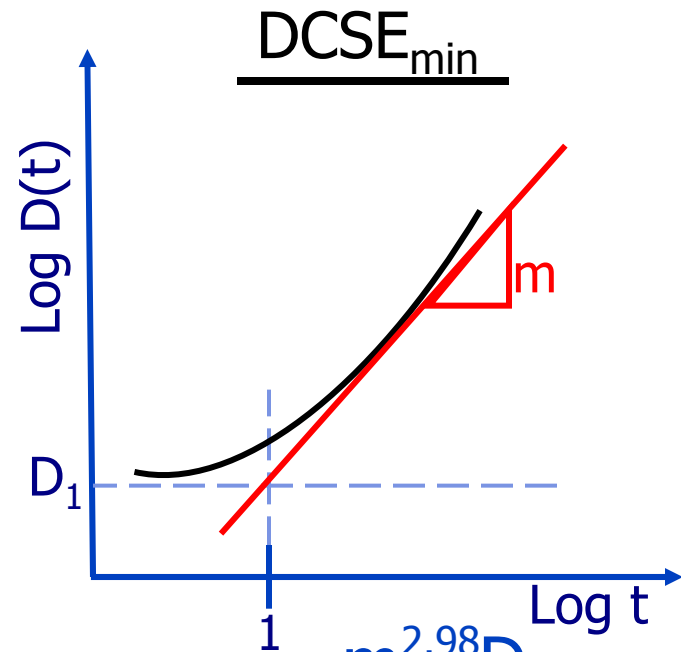


Energy Ratio Concept

- The $DCSE_{HMA}$ has to be greater than the $DCSE_{min}$ for good cracking performance:



- $DCSE_{HMA} = \text{AREA}$

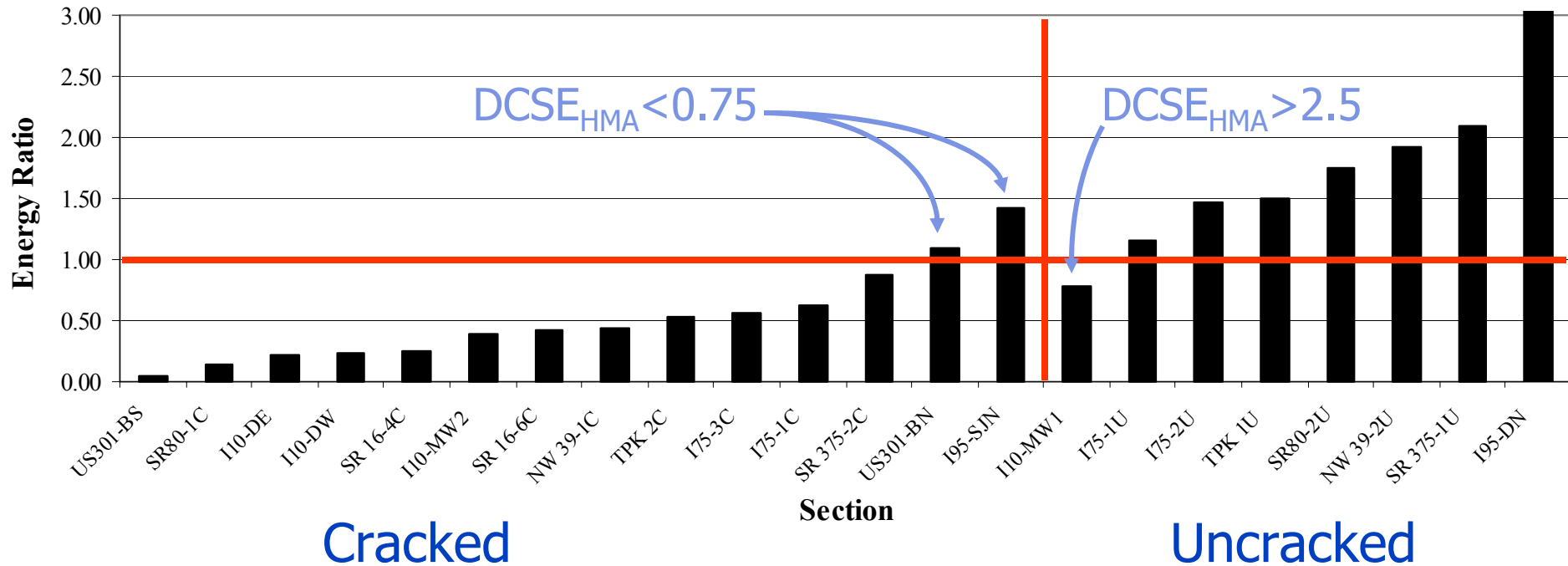


- $DCSE_{min} = \frac{m^{2.98} D_1}{A}$

ENERGY RATIO = $\frac{DCSE_{HMA}}{DCSE_{min}} > 1$

Energy Ratio Results

- Examined all sections
- Performance criteria: $ER > 1$; $DCSE_{HMA} > 0.75$



Summary & Conclusions

- Volumetric properties are not a good predictor for cracking performance
- Verified the importance of mixture properties and pavement structure in predicting cracking performance
- HMA fracture mechanics properly accounts for effects of mixture properties. The relative cracking performance predicted agrees with field observations



Summary & Conclusions

- Identified and defined a set of criteria that can predict mixture cracking performance:
 - $ER > 1$
 - $DCSE_{HMA} > 0.75$
- Verified the requirements with previous test sections
- No single property can be an accurate performance predictor; properties are interrelated and we need to consider them as a system

